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#### FINAL REPORT

to National Aeronautics and Space Administration Goddard Space Flight Center Greenbelt, MD

NASA Contract Number NAS5-30514

#### EARTH'S EXTERNAL MAGNETIC FIELDS AT LOW ORBITAL ALTITUDES

Period: May 18, 1988 - May 18, 1990

### Principal Investigator:

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### EARTH'S EXTERNAL MAGNETIC FIELDS AT LOW ORBITAL ALTITUDES

Final Report Period: 18 May, 1988 to 18, May 1990

Contract NAS5-30514

Submitted by D. M. Klumpar Lockheed Palo Alto Research Laboratories

#### INTRODUCTION AND BACKGROUND

Under our June, 1987 proposal entitled "Magnetic Signatures of Near-Earth Distributed Currents" we proposed to render operational a modeling procedure that had been previously developed to compute the magnetic effects of distributed currents flowing in the magnetosphere-ionosphere system. After adaptation of the software to our computing environment we would apply the model to low altitude satellite orbits and would utilize the MAGSAT data suite to guide the analysis. A contract to conduct this effort was awarded to LMSC in May, 1988.

During the first year basic computer codes to run model systems of Birkeland and ionospheric currents and several graphical output routines were made operational on a VAX 780 in our research facility. Software performance was evaluated using an input matchstick ionospheric current array, field-aligned currents were calculated and magnetic perturbations along hypothetical satellite orbits were calculated. The basic operation of the model was verified. Software routines to analyze and display MAGSAT satellite data in terms of deviations with respect to the earth's internal field were also made operational during the first year of effort. The complete set of MAGSAT data to be used for evaluation of the models was received at the end of the first year. A detailed annual report in May 1989 described these first year activities completely. That first annual report is included by reference in this final report.

This document summarizes our additional activities during the second year of effort under the contract, describes the modeling software and its operation, and includes as attachment the deliverable computer software specified under the contract.

#### MODEL DESCRIPTION

#### Description of Modeling Procedure

The modeling software described below is designed to facilitate studies of the contributions that ionospheric and magnetospheric currents make to the magnetic fields measured on low altitude polar orbiting satellites. Emphasis is placed on high latitude current systems because, as previously has been shown, large and highly variable perturbations of the geomagnetic field are associated with high latitude auroral phenomena. The routines compute the vector magnetic contributions at any point that arise from currents flowing in the ionosphere and along the magnetic field into the magnetosphere. The contribution due to a distant equatorial Ring Current is also included.

The basic modeling codes take, as input, an array of ionospheric currents distributed over a specified region of the polar ionosphere. Figure 1 illustrates the basic grid cell concept and shows the distribution of current locations for a coarse setup of 4 latitude cells and 12 longitude cells. This 4x12 array is illustrative for the purpose of showing how the grid cells, the ionospheric currents, and the Birkeland currents relate to one another. In actual use of the model a much finer grid consisting of many more grid cells would be employed. The view is looking down upon the polar regions with the earth's diple axis protruding from the center of the diagram. Magnitude and direction of the horizontal currents are specified for each point on a spherical surface at some altitude above the earth's surface. This altitude constitutes the base of the cell. The horizontal currents are shown in Figure 1 by arrows at the center of each grid cell. Each such horizontal current specification thereby locates a current cell, the bounds of which are determined by the density of current specification points. The latitude extent of the entire current system is bounded at the northern and southern boundaries by the first and last cell boundaries. In this illustration the latutude range is from 70° to 50°.

Currents flowing outward and inward along magnetic field lines provide the sources and sinks for the horizontal ionospheric currents. These field-aligned currents constitute the Birkeland current system. In practice these currents are represented by straight filaments which are tangent to the magnetic field lines at the ionosphere (the base of the cell) and are three earth radii in length. A more complex model, in which the field-aligned filaments curved with the magnetic field lines all the way to the equatorial plane was tested. The increased complexity made a barely discernable difference in the final result and because of this reason and in view of the increased computation time the simpler concept was adopted. Once the ionospheric currents have been specified and the region boundaries have been determined the modeling codes compute the Birkeland currents at each cell boundary as required for the preservation of current continuity. In Figure 1 these currents are shown as circles located at each cell boundary. Each circle encloses about 90% of the kurtically distributed current.

The magnetic field at any point is the vector sum of the contributions from all current elements in the system. Once the currents have been defined as described above the software can compute the magnetic field at any location. In practice, as will be described below, we compute the magnetic field along a satellite orbit through (and above) the current system so as to be able to relate the field signatures observed in real satellite data to the model fields.

A very important aspect of the model is the representation of the currents. The current elements are like current carrying wires, in that they have thickness. But unlike wires, they have smoothly varying cross-sectional current density. The current density in each element is platykurtically distributed over the cross-section of the current element. The kurtic representation is one which varies as the hyperbolic secant of the square of the distance from the center of the element. This gives a more realistic representation of the currents and prevents large and sudden transitions of the magnetic field.

#### Software Codes

The Fortran source codes revived under this contract and submitted as deliverables items are attached as Attachment B. The suite of Fortran source code to directly carry out the modeling and display consists of more than 1500 lines of code. The component codes are listed in the following table. Also shown in the table are the input and output data files.

Table 1: Magnetic Modeling Routines

INPUT	SOFTWARE CODE	OUTPUT	<u></u>
Run-time	SCURDIS	DIS.DAT	
DIS.DAT + run-time	SAMPLT	Graphics	
DIS.DAT + run-time	SBRKPLT	Graphics	
DIS.DAT + run-time	SBRKALC	MAĞ.DAT	
MAG.DAT + run-time	SBRKPLT	Graphics	

#### A functional description of each code follows:

SCURDIS This Fortran routine sets up the current system with the input currents. The routine calculates all the necessary geometric parameters needed to specify the current elements and their location in space and writes these parameters along with the current magnitudes in the output file DIS.DAT. Runtime input information required for the code to run consists of specifying the number of cell rings, number of longitude sectors, inner and outer co-latitude boundaries of the current system, maximum current filament radius and latitude thickening exponent.

SAMPLT This is a graphical output routine that plots on a polar projection all Birkeland currents required to complete continuity with the specified ionospheric currents. The circlegram shows the magnitude and location of the Birkeland current filaments. Input data file is the DIS.DAT file produced by SCURDIS. Additional runtime input includes a divisor which controls the current represented by each line of the circlegram. Output is graphical and is delivered to one of nine possible output devices specified under runtime control. The format of this output will be dependent upon facilities at the operator site. Standard Tektronics 4010 and laser postscript output are among possible options.

SBRKPLT This is a graphical output routine that plots on a polar projection all horizontal ionospheric currents in the input system. The vectors show the location, magnitude and direction of each cell current filament. Input data file is the DIS.DAT file produced by SCURDIS. Additional runtime input includes a multiplier which controls the length of the vector in terms of the current magnitude. Output is graphical and is delivered to one of nine possible output devices specified under runtime control. The format of this output will be dependent upon facilities at the operator site. Standard Tektronics 4010 and laser postscript output are among possible options.

SBRKALC This routine calculates measurement positions for a specified satellite orbit and calls SMAGMOD. Input data file is the DIS.DAT file produced by SCURDIS. Additional runtime input includes the orbital altitude of the satellite, it's inclination and local time location of the orbit plane. The density of measurement points along the orbit is also controlled by runtime input. A switch is provided at input to allow the user to select only a part of the global currents to determine the individual contributions of various parts of the current system to the magnetic field. It is also possible to compute

low latitude magnetic perturbations. This routine calls SMAGMOD. Output is written to file MAG.DAT.

SMAGMOD This routine calculates, for each measurement location, the net vector magnetic field due to all of the distributed currents. It is called by SBRKALC. At each measurement point the vector sum of the individual contributions from each and every current element in the system is computed and returned to SBRKALC along with the magnitude of the Birkeland current at each measurement point.

SBRKPLT This is a graphical output routine that plots the three components of the magnetic perturbation at each measurement point along the satellite orbit specified in SBRKALC. Basic input array is provided by MAG.DAT. User runtime choices allow the displayed perturbations to be cast into one of four coordinate representations: XYZ, NEV, SDV, and ABZ. Output is graphical and is delivered to one of nine possible output devices specified under runtime control. The format of this output will be dependent upon facilities at the operator site. Standard Tektronics 4010 and laser postscript output are among possible options.

#### Running a Model

As an example of the model routines in actual use we illustrate in the following a complete run of the modeling system. The output is shown in Figures 2-4. A complete run through the system starts by running SCURDIS to set up the ionospheric input currents. In the version of SCURDIS contained in this report, up to 20 latitude cells and up to 24 longitude cells may be used. Each cell contains a specification for the vector ionospheric current at that location. Since Hall and Pederson conductivities are often used in physical descriptions of the auroral ionosphere and since ionospheric currents are often discussed in terms of the eastward and westward electrojects, we choose in practice to specify the ionospheric currents by their E-W and N-S components. The data file produced by SCURDIS contains information regarding the location, direction, and magnitude of the currents to be passed on to subsequent programs in the sequence.

Once the complete current specification has been set up by CURDIS, two plotting programs (SAMPLT and SCURPLT) are available to view the ionospheric and the resulting field-aligned currents. Figure 2 depicts the input ionospheric current system used for this example. Looking down upon the earth's polar region the figure shows, on a local time vs latitude polar projection, the ionospheric current vectors at each grid cell input point. This current system is the direct input for the model. In this model run a cell matrix of twenty latitude rings by 24 longitude sectors is used to represent an ionospheric current that has a strong eastward electrojet throughout the post noon sector and into the morning sector. The current is restricted to the latitude range from 57 to 85 degrees. This output is produced by the SCURPLT program.

The model calculates the field-aligned currents required to maintain current continuity. For this example the resulting field-aligned current distribution through an imaginary spherical shell above the ionospheric currents is shown in Figure 3. Field-aligned currents flow in and out at each grid point as required to maintain current continuity. Since there is a string divergence in the ionospheric currents along the noon meridian (see Figure 2) there is a strong downward field-aligned current at this location as seen in Figure 3. Current flows upward or downward along magnetic field lines as indicated by the horizontal or vertical hatching, respectively.

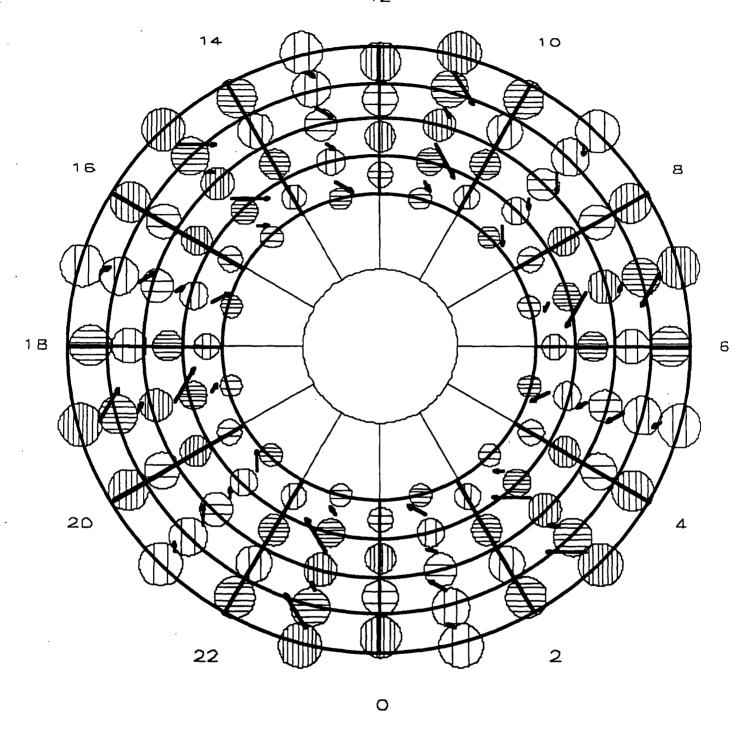
The product of ultimate interest is the magnetic field at any point. The magnetic perturbation code (SBRKALC) is set up to receive a specified satellite orbit and to

calculate the magnetic field perturbations at points along that orbit for one of several possible coordinate systems. SBRKALC is given the orbital parameters for the satellite and calculates the magnetic perturbations due to any one or all parts of the current system. The resulting information is written to the file MAG.DAT which in tern may be plotted using the program SBRKPLT. As an example, Figure 4 illustrates the magnetic field perturbations due to the model current system shown in Figures 2 and 3 that a satellite at 450 km altitude would see as it passes over the current system in an evening to morning orbit as shown in the upper right hand clock dial. Perturbations are shown for the three vector components northward (N), eastwardward (E) and vertical (V). The bottom panel shows the magnitude of the local field-aligned currents that the satellite passes through while the magnetic perturbations in the upper three panels are due to all of the currents in the entire system. The coordinate system for output of the perturbations is selected at runtime in BRKPLT.

#### Other activities during second year

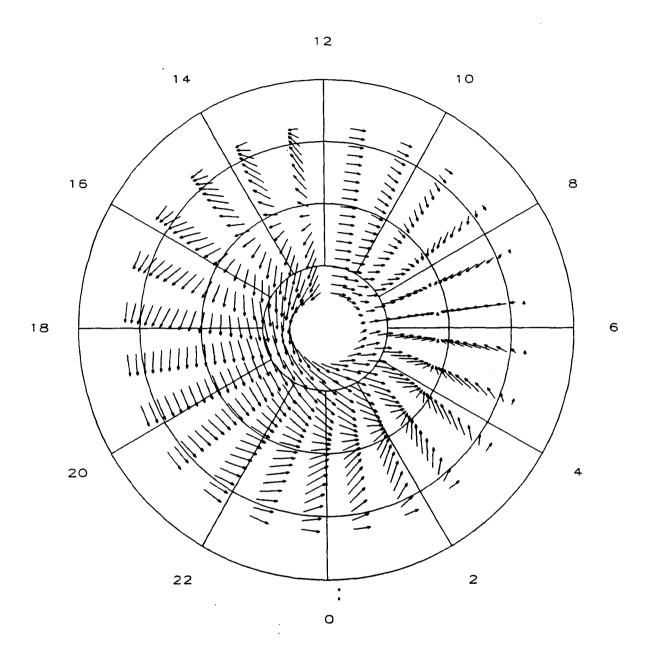
An abstract was submitted, and accepted for presentation, at the spring 1990 American Geophysical Union meeting of results of the investigations carried out under this contract. The paper is entitled, "A Method for Computing Magnetic Perturbations at Satellite Altitude due to Distributed Currents in the Ionosphere and Magnetosphere". The paper emphasizes the capabilities of the model as a tool to examine the relative contributions of the magnetic perturbations which result from the various components of the current distribution. The capability to selectively "switch on" parts of the current system while evaluating the magnetic perturbations is a powerful tool for understanding the sources of the magnetic perturbations seen on earth-orbiting satellites. In the computer model there are four distinct current components: ionospheric N-S, ionospheric E-W, field-aligned, and ring current. Of course the currents themselves are intimately tied together by the requirement for current continuity and cannot be independently controlled without creating a physically impossible situation. The magnetic contribution, however, of each of the four can be selectively switched on to determine the effect of any one of them on the magnetic field at any measurement point. This provides a unique analysis tool that the natural environment cannot provide. It allows us to examine singularly the effect on the magnetic perturbations seen at the satellite due to each major component in the global current system. Such a diagnostic is an indispensable tool for understanding the behavior of the magnetic perturbations in orbit. A copy of the abstract is attached to this report as Attachment A.

Most of our progress with respect to the MAGSAT data was directed toward getting the data tapes and modifying our MAGSAT analysis routines to run on the VAX 780. The software has been transported to the VAX and is running successfully. Several figures in our first annual report showed sample plots from these analysis routines, and will not be repeated here.



### DISTRIBUTION OF CURRENTS

FIGURE 1

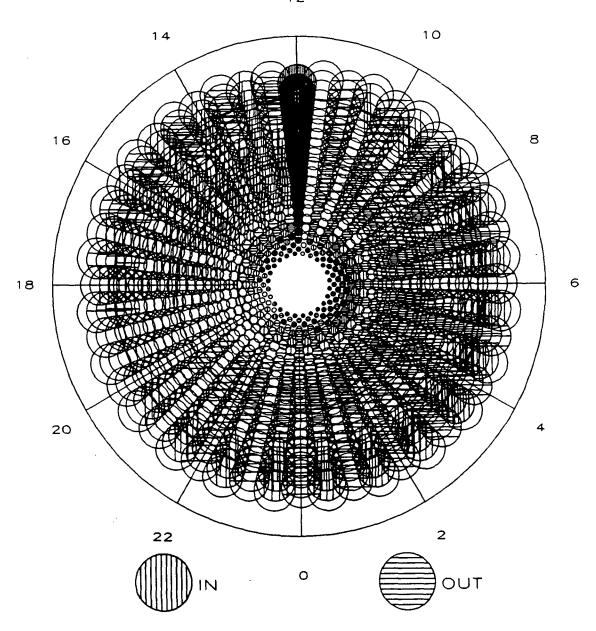


DISTRIBUTION OF IONOSPHERIC CURRENTS



FIGURE 2

12



DISTRIBUTION OF FIELD ALIGNED CURRENTS

CURRENT IS 500.00 AMP/LINE

50005332024

18-MAY-90 21:34:59 MODEL:[SIMPLE]DIS.DAT;36 18-MAY-1990 21:13:10.7

FIGURE 3

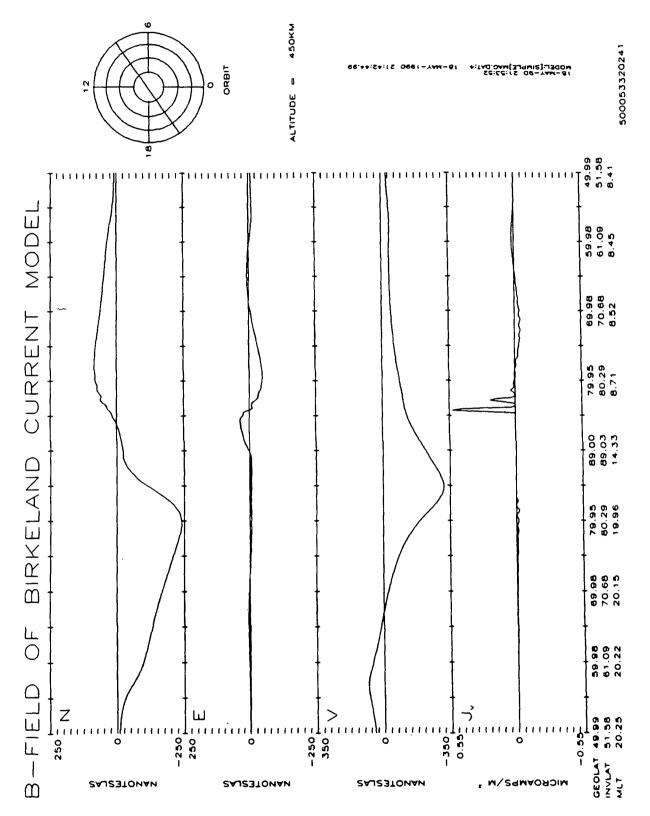


FIGURE 4

ATTACHMENT A
Abstract of paper submitted to Spring 1990
American Geophysical Union Meeting

A Method for Computing Magnetic Perturbations at Satellite Altitude due to Distributed Currents in the Ionosphere and Magnetosphere

D. M. Klumpar (Lockheed Palo Alto Research Laboratory, Palo Alto, CA, 94304; 415-424-3288; SPAN mail LOCKHD::KLUMP)

Low altitude magnetic survey satellites respond to the main magnetic field, to crustal anomaly fields, and to fields produced by currents in the ionosphere-magnetosphere system. One sub-discipline of space sciences endeavors to describe the space currents and relate them to processes in the magnetosphere and ionosphere. It is generally assumed that the entire observed magnetic perturbation is due to currents close to the satellite with a simple planar sheet current geometry. Given these assumptions one obtains an approximation for the local field-aligned currents. Contributions from distant sources are ignored. In the field of terrestrial geomagnetism the space currents represent a large temporally varying source of contaminating signal that must be removed to deduce the main field and/or crustal anomaly fields. Steep gradients due to local effects are readily recognized but larger-scale perturbations are a severe cause of inaccuracies. We illustrate here the use of a modeling routine, which has application to each of the above disciplines. The technique computes the magnetic field along a satellite orbit due to distributed electrical currents in the ionosphere and magnetosphere. It takes as input a description of the distributed currents over the entire high latitude ionosphere and computes the magnetic contribution at each point from the ensemble of currents in the system. Using this technique we input realistic current distributions and calculate the resulting magnetic perturbations along a satellite orbit. The modeling software is useful as a research tool for analyzing the relative contributions of local and more distant currents at a satellite and therefore generally as a tool in understanding the sources of the magnetic purtabation signatures. Various portions of the input currents can be controlled independently, or turned off completely, so as to allow a versatility to "experiment" that is not found in nature. Since the model requires an ad hoc input current system it is not, in its present form, suitable for uniquely determining the currents that give rise to a specific measured magnetic perturbation profile. For that one requires a solution to the inverse problem. As an application of the technique we show distributed current systems which produce magnetic signatures that compare favourably with actual Magsat measurements and illustrate how the different components of the current system individually contribute to the magnetic perturbation.

- 1. 1990 Spring Meeting
- 2. 000895585
- 3. (a) D. M. Klumpar Dept 91-20/B255 Lockheed 3251 Hanover Street Palo Alto, CA 94304
  - (b) 415-424-3288
- 4. **GP**
- 5. (a) GP08 Magnetic
  Disturbances: Separation,
  Modeling and Applications
  - (b) 2708 Current Systems, 1594 Instr and Techniques
- 6.
- 7. 0%
- 8. Invoice \$60 to PO#
  ZAP22568 (Copy attached)
  Attn: Lois Fulbright
  Technical Information
  Dept 90-11, Bldg 201
  3251 Hanover Street
  Palo Alto, CA 94304
  Phone 415-424-2810
- 9. C
- 10. none
- 11. No

ATTACHMENT B FORTRAN Source Codes Magnetic Field Model

# SCURDIS SOURCE CODE

```
SCURDIS.FOR revision history, Summer, 1988
              John L. Jamison, for Dr. DM Klumpar
              Lockheed Palo Alto Research Laboratory
C
c
              0/91-20 B/255
C
   6/29/88
              JLJ
                    made this "Simple" version of curdis
                    added INCLUDE for standardization of data decl.
                                       input promise
Ø
                    changed AMPS to amp
a
   6/28/88
a
              JLJ
                    added "Units" in value input prompts, and
                    input-verification code
a
   6/28/88
              JLJ
                    changed E-W currents in loop 40000
C **** CURDIS DEFINES A CURRENT DISTRIBUTION ARRAY AND
C **** PUTS IT INTO A DATA FILE, DIS.DAT
     subroutine SCURDIS (inter, prumt, pruml, poll, poll, prf, pdf, proode)
       include 'model:[simple]sbrk.inc'
                                       DIMENSION CL (2,21)
     DIMENSION TCL(2,21)
     DIMENSION CLI (2,21), TMU (2,21)
     REAL*4 LAMBDA
     DATA PI / 3.14159265 /
     DATA RE / 6371000. /
     DATA ALTI / 120000. /
C
     integer pount, pount, pacode
     real prf,pdf,poll,pol2
     if (inter.eq.0) then
       numl-pouml
       nust-pount
       rimpri
       df-pdf
       all-pall
       al2=pal2
       ncode-pacode
       goto 2000
     endif
     write (5,*)
     write (5,*) ' CURDIS.EXE'
     write (5,*)
00999 WRITE (5,01000)
01000 FORMAT ('$Enter number of Cell Rings [ INTEGER, 1.. 20 ] : ')
     READ (5,+) NUME
     18 (numt.lt.l.or.numt.gt.20) goto 999
01009 WRITE (5,01010)
01010 FORMAR ('$Enter number of cells per 360 deg longitude '
        '[ INTEGER, 1..24 ] : ')
     READ (5, *) WORL
     if (numl.It.1.or.numl.gt.24) goto 1009
```

```
01019 WRITE (5,01020)
01020 FORMAT('$Enter inner and outer colatitudes of ring'
              '[ REAL, 0.0 .. 90.0 ] : ')
     READ (5,*) CL1, CL2
     if ((cll.lt.0.0.or.cll.gt.90.0).or.(cl2.lt.0.0.or.cl2.gt.90.0))
     * goto 1019
C
     WRITE (5,01040)
01040 FORMAT('$Enter max radius of current filaments'
    * '[REAL, maters]:')
     read (5,*) rf
     WRITE (5,01050)
01050 FORME ('SEnter latitudinal thickening exponent : ')
     READ (5, *) DF
     WRITE (5,01060)
01060 FORMAT ( * (Rater model number : *)
READ (5.*) ECODS
 2000 continue
C
**** LOOP 10000 DEFINES THICKNESS OF CURRENT FILMENTS:
C **** FOR F-A CURRENTS SUPPLYING E-W CURRENTS ON I = 1;
 **** FOR N-S CURRENTS ON I = 2;
C **** FOR E-W CURRENTS ON I = 3.
C
     DO 10000 I = 2, 4
        DO 10000 J = 1, NUMP
          DO 10000 K = 1, NUML
             TP(I,J,K) = 1.089/((((J-.5)*(CL2-CL1)))
                         /MUMT + CL1)/CL2)**DF)*(RF**2))
    1
10000 CONTINUE
C
C *** LOOP 20000 DEFINES THICKNESS OF CURRENT FILAMENTS
C **** FOR F-A CURRENTS SUPPLYING M-S CURRENTS.
C
     H = HUM2 + 1
     DO 20000 J = 1. M
        DO 20000 K = 1, MUMIL
          27 (1, J, K) = 1,089/(((((J-1)*(CL2-CL1)/NUME + CL1))
                     /CL2) **DF) * (RF**2) )
20000 CONTINUE
 *** LOOPS 30000 AND 40000 DEFINE CURRENT PER LOOP FOR N-S AND E-W RESP.
C
C
     DO 30000 J = 1, NUMT
        DO 30000 K = 1, NUML
          8 = -1./2.
          IF (K.GT.MUML/2.) 8 = 1./2.
          amp (1, J, K) # $
30000 CONTINUE
     DO 40000 J = 1, NUMT
        DO 40000 K = 1, NUML
                                                                or spinor
          Sa-.5
          IF (K .GT. 12.*WUNCL/24.) 8 = 0.5
          amp(2,J,K) = 8
40000 CONTINUE
```

```
C **** LOOPS 50000 AND 60000 DEFINE LENGTH OF CURRENT FILAMENTS
C **** AND THEIR LOCATION IN SPACE
      DO 50000 I = 1, 2
        DO 50000 J = 1, N
           50000 J = 1, H

CL(I,J) = ((CL2-CL1)*(I*J-1)/(I*NUNT) + CL1)*PI/180.

SCL(I,J) = SIM(CL(I,J))

CIJ(I,J) = COS(CL(I,J))
           TCL(I,J) = TAM(CL(I,J))
           CLI(I,J) = ATAM(2./TCL(I,J))
           CMU(I,J) = SIM(CLI(I,J) - CL(I,J))
            SMU(I,J) = COS(CLJ(I,J) - CL(I,J))
           THU (I, J) = 1./TAM (CLI (I, J) - CL(I, J))

REF (I, J) = (RR + ALEI) + (CCL(I, J) - SCL(I, J) / THU (I, J))

PR (I, J) = (PR - ALEI) + (CCL(I, J) - SCL(I, J) / THU (I, J))
           RB(I,J) = (RE + ALTI) *SCL(I,J) /SMU(I,J)
           RT(I,J) = (RE + ALTI) +3.
50000 CONTINUE
        60000 H = 1, HIMT
RSI(E) = (RE + N.FI)*(COS(CL(1.E)*CL(2.E)))/CCL(2.E)
      DO 60000 K = 1, MDAT
        RI(1,K) = RSI(K)*SCL(2,K)
                  - (RE + ALTI) *SIM(CL(2,K) - CL(1,K))
        RI(2,K) = RI(1,K) + 2.*(RE + ALTI)
        *SIN(CL(2,K) * CL(1,K))

BER(E) = RE + ALTI

REJ(E) = RES(K) *TAN(PI/NUGL)
60000 CONTINUE
C **** LOOP 70000 DEFINES THE RING CURRENT
C
     RINGA-4.*RE
      RIMCR-4. *RE*TAM (PI/MUML)
      DO 70000 I=1, NUML
        TPR(I)=1.009/(1000**2)
        AMPR(I)=1.
70000 CONTINUE
C
OPER (UNIT-1, MAME='DIS.DAT', TYPR='MEN')
MRITE (1,*) MCODE, DF
WRITE (1,*) CL1. CL2
      WRITE (1,*) NUME, NUME.
      WRITE (1,+) (((TP(I,J,K), K=1,NUML), J=1,M), I=1,4)
      WRITE (1, *) (((amp(I,J,K), K=1,MUML), J=1,MUMT), I=1,2)
     WRITE (1,*) ((RIF(I,J), J=1,H), I=1,2)
WRITE (1,*) ((RE(I,J), J=1,H), I=1,2)
WRITE (1,*) ((RE(I,J), J=1,H), I=1,2)
      WRITE (1, *) (REI(K), K-1, NUMT)
      WRITE (1, *) (REE(I), I=1, NUMT)
      WRITE (1,*) (REJ(I), I=1, NUMT)
      WRITE (1,*) ((RI(I,J), J=1,NUMT), I=1,2)
      WRITE (1,*) ((SCL(I,J), J=1,N), I=1,2)
      WRITE (1,*) ((CCL(I,J), J=1,H), I=1.2)
      MRITE (1,*) ((SMU(I,J), J=1,N), I=1,2)
      WRITE (1, *) ((CMU(I, J), J=1, N), I=1,2)
      WRITE (1,*) RINGA, RINGB
      MRITE (1,*) (TPR(I), I=1, NUML)
      MRITE (1, *) (AMPR(I), I=1, NUML)
      CLOSE (UNIT=1)
```

RETURN
END

program scurdis it
 implicit none
 call scurdis(1,,,,,)
end

## SAMPLT SOURCE CODE

```
SAMPLT
                       Birkfield Current Ampere Plot
c
C
                       JL Jamison, for DM Klumpar
_
                       Lockheed Palo Alto Research Laboratory
C
                       O/91-20 B/255
C
   Revision History
C
         2-Jul-88
                               cleaned up input prompting
                               added SBRK. INC to standardize declarations
        30-Jun-88
                       ليلل
C
C **** AMPLY SHOWS CURRENT FLOWING THROUGH THE SURFACE OF A SPHERE
C **** JUST ABOVE THE IONOSPHERIC CURRENTS.
C **** BACE CIRCLE REPRESENTS A FIELD ALIGNED CURRENT FILAMENT AND
C **** ABOUT 90 PERCENT OF THE PLATICURTICALLY DISTRIBUTED CURRENT
C **** IS THEREIN ENCLOSED.
C **** BACE LINE IN ONE OF THESE CIRCLES REPRESENTS ONE AMP (NUMBER
C *** OF LINES + OR - .5 IS CURRENT).
CORRE
C
      subroutine samplt (inter, pfmum, pdiv)
       include 'model: [simple] abrk.inc' ! JLJ
      DIMENSION AMP (2, 20, 24), TP (4, 21, 24)
C
      character *2 fnum, pfnum
      character #11 darray /'DIS.DAT;
     integer inter
      real pdiv
      REAL+4 INCL, MLT
     DATA PI / 3.14159265 /
     DATA CF / 1.25948-6 /
     DATA INCL. THTA / 'INCL', 'THTA'
C
write (6,997)
00997 format ('4')
     write (6,*)
                     SAMPLT . EXE
                                   Birkeland Field-Aligned
     * //'Current Distribution'
     write (6,998)
00998 format ('3')
     if (inter.eq.0) then
         form (1:2) -pform (1:2)
         div = pdiv
         goto 2000
     endif
     WRITE (6,01000)
01000 FORMAT ('SEnter DIS.DAT version number [ Integer ] : ")
     READ (6,01010) FNUM
01010 FORMAT (2A)
     WRITE (6,01020)
01020 FORMAT ('SEnter direlegram DIV factor [ Real ] : ')
     READ (6,*) DIV
02000 DARRAY (9:10) = FNUM (1:2)
```

```
if (inter.eq.1) then
       write (6,*) 'File : ', darray(1:10)
       write (6,*) 'Div : ', div
       write (6,*)
     endif
     CALL CALCHE (X,Y,2,0)
     CALL CALCHP (X,Y,0,2)
     XORG = 5.6
     YORG = 5.5
     CALL CALCHP (XORG, YORG, 0, 3)
     CALL GRAIN(0.0)
     call putinfo(darray(1:11),7.8,1.5,.1,.false.)
C
OPEN (UNIT-1, NAME-DARRAY, TYPE-'OLD')
     READ (1,+) MCODE
     READ (1,*) CL1, CL2
     READ (1, *) NUMT, NUML
     M - NUMT + 1
     READ (1,*) ((TP(I,J,K), K=1,NUNL), J=1,N), I=1,4)
     READ (1,*) (((AMP(I,J,K), K=1,NUML), J=1,NUMT), I=1,2)
     CLOSE (UNIT=1)
     M = MUMT + 1
     DO 20000 MT = 1. 2
        DO 20000 I = 1, H
          DO 20000 J = 1, NUMI.
C
C **** THIS SECTION CALCULATES THE CURRENT PER FILAMENT
C
             IF ((MT .EQ. 2) .AND. (I .EQ. N)) GO TO 20000
             T = ((I-1./MT) * (CL2-CL1)/MUNT + CL1)/40.
             XL = -4.5*F*COS(2.*(J+NT/2.-1.)*PI/NUML)
             YL = -4.5*P*SIN(2.*(J+NT/2.-1.)*PI/NUML)
             PAICP = AICP(1,1,J)
             IF ((MT .EQ. 2) .AND. (J .LT. WUNL))
             \mathbf{FAMP} = \mathbf{AMP}(2,\mathbf{I},\mathbf{J+1}) - \mathbf{AMP}(2,\mathbf{I},\mathbf{J})
    1
             IF ( (NT , EQ. 2) .AND, (J , EQ. NUML))
    1
             \mathbf{FAMP} = \mathbf{AMP}(2,1,1) \sim \mathbf{AMP}(2,1,\mathbf{NUML})
             IF ((NT .EQ. 1) .AND. (I .GT.1))
             FAMP = AMP(1, 1, J) - AMP(1, I-1, J)
             IF ((NT .EQ. 1) .AND. (I .EQ. N)) PAMP -- AMP (1, NUMT, J)
             IF (FAMP .EQ. 0.) GO TO 20000
C **** LOOP 21000 CALCULATES THE RADIUS OF EACH FILAMENT
C **** AND DRAWS THE CIRCLE REPRESENTING IT.
C
             RF = SQRT (1.089/TP (NT, I, J))
     CALL CALCID (XL, YL, 0, 1)
     PRAD=RF*CF
     CALL CALCID (XL, YL, 1, -5)
     CALL ARC (PRAD, 0, , 360.)
     CALL CALCID (XL, YL, 0, -5)
C **** LOOPS 22000 AND 23000 DRAW THE LINES IN BACH CIRCLE THAT
```

```
C **** SHOW THE CURRENT IN EACH FILAMENT, 22000 FOR IN AND 23000 FOR OUT.
С
              IF (ABS (FAMP/DIV) .LT. .05) GO TO 20000
              NLINE = INT(ABS(FAMP*10./DIV) + .5)
              IF (FAMP .LT. 0.) GO TO 20300
              DO 22000 L = 1, NLINE
                 XW = RF*CF*SQRT(1, -(1, -L/((NLINB+1)/2,))**2)
                 Y = YL + RF*CF*(1,-L/((NLINE+1)/2,))
                 CALL CALCHY (X,Y,0,1)
                 X = XL + XW
                 Y = YL + RF*CF*(1.-L/((NLINE+1)/2.))
                 CALL CALCOD (X, Y, 1, 1)
              CONTINUE
22000
              IP (FAMP .CT. 0.) GO TO 20000
20300
              DO 23000 M = 1, NLIME
                 YW = RF*CF*SQRT(1.-(1.-M/((NLINE+1)/2.))**2)
                 X = XL + RF*CF*(1.-M/((NLINE+1)/2.))
                 Y - YL - YW
                 CALL CALCOP (X, Y, 0, 1)
                 X = XL + RP*CP*(1,-M/((MLINR+1)/2.))
                 X = X\Gamma + XM
                 CALL CALCHO (X,Y,1,1)
              CONTINUE
23000
20000 CONTINUE
C **** LOOPS 30000 AND 40000 DRAW THE LATITUDE CIRCLES AND
C *** MLT LIMES AND LARRLS RESPECTIVELY.
     CALL CALCED (0.,0.,0,1)
     DO 30000 I = 1, 4
       PRAD=1.125*I
       CALL ARC (PRAD, 0., 360.)
30000 CONTINUE
C
     DO 40000 I = 1, 12
        TH = (I-1)*PI/6.
        ST - SIN(TH)
        CT = COS (TH)
        XL = 4.5*CT
        YL = 4.5*ST
        X = XL - 3.375 CT
        Y = YL - 3.375*ST
        CALL CALCER (X, Y, 0, 1)
        X = XL
        Y - YL
        CALL CALCID (X,Y,1,1)
        MLT = 2.*(I-1)
        XX = XI_1 + .7*CT + .105
        YM = YL + .5*87 - .07
        IF (MLT .GT. 9) YM = YN - .14
        CALL NUMBER (XM. YM. . 21, MLT, 90., -1)
40000 CONTINUE
C
C **** LOOP 50000 DRAWS TWO REPRESENTATIVE FILAMENT CROSS-SECTIONS
C **** ONE SHOWING CURRENT IN, THE OTHER, CURRENT OUT, EACH HAS
  **** A RADIUS OF 400000 METERS AND A CURRENT OF TEN AMPS.
      ROP = 400000.
```

```
DO 50000 I = 1, 2
         GO TO (50010,50020) I
50010
         XL = 5.3
         YL = -2.5
         GO TO 50030
50020
         XL = 5.3
         YL = 1.9
50030
         PRAD=ROP*CF
         CALL CALCID (XL, YL, 0, 1)
         CALL ARC (PRAD, 0., 360.)
         GO TO (50040,50050) I
         DO 52000 J = 1, 10
50040
            XW = ROP*CF*SQRT(1.+(1.+J/5.5)**2)
            X = XL - XM
            Y - YL + ROP*CF* (1.-J/5.5)
            CALL CALCIE (X,Y,0,1)
            X = XL + XW
            Y = YL + ROP*CF*(1.-J/5.5)
            CALL CALCID (X,Y,1,1)
52000
         CONTINUE
         GO TO 50000
50050
         DO 53000 J = 1, 10
            YW = ROP*CP*SORT(1.-(1.-J/5.5)**2)
            X = XL + ROP * CF * (1.-J/5.5)
            Y = YL - YW
            CALL CALCID (X.Y. 0.1)
            X = XI, + ROP*CF*(1.-J/5.5)
            Y = YL + YW
            CALL CALCIER (X, Y, 1, 1)
53000
         CONTINUE
50000 CONTINUE
COBBBB
      CALL SYMBOL (6.7, -5.07, .28, 22HDISTRIBUTION OF FIELD ,90.,22)
      CALL SYMBOL (999., 999., .28, 16HALIGHED CURRENTS, 90., 16)
      CURR-DIV/10.
      CALL SYMBOL (7.5, -5.21, .14, 11BCURRENT IS , 90., 11)
      CALL MUMBER (999, 999., .14, CURR, 90., 2)
      CALL SYMBOL (999., 999., .14, 9H AMP/LINE, 90., 9)
      CALL SYMBOL (5.5, -1.9, .28, 2NIM, 90., 2)
      CALL SYMBOL (5.5, 2.5, .28, 3HOUT, 90.,3)
      RCODE - MCODE
      CALL MUMBER (8.0, -5.07, .14, RCODE, 90.,0)
      CALL NUMBER (999, , 999., .14, CL1, 90.,0)
      CALL NUMBER (999., 999., .14, CL2, 90., 0)
      RUMT-MUMT
      CALL NUMBER (999., 999., .14, RUMT, 90., 0)
      RUNG-MUNG.
      CALL NUMBER (999., 999., .14, RUML, 90., 0)
      CALL PAUS
      CALL CALCID (X,Y,1000,2)
      RETURN
      END
      program samplt it
        call samplt (1,' ',0.0)
        stop
      end
```

# SCURPLT SOURCE CODE

```
SCURPLT FOR
                         Birkland Current Distribution Plotter
c
                      JT. Jamison. for DM Klumpar
c
                      Lockheed Palo Alto Research Laboratory
c
                      0/91-20 B/255
c
c
c
       Revision History
a
        12-Jul-88
                      JIJ made into callable procedure
a
        2-Jul-88
                      JIJ
a
                              cleaned up input prompts
       30-Jun-88
                      JLJ
                              added 'SBRK.INC' to standardize declarations
C **** CURPLY SHOWS THE CURRENT VECTORS IN THE IONOSPHERE
subroutine scurplt (inter.pfnum.pour)
       include 'model: [simple] abrk.inc'
     character*11 darray /'DIS.DAT: '/
     character*2 fnum, pfnum
     integer*4 inter
     REAL+4 MLT, pour
     DATA PI / 3.14159265 /
     write (6,997)
0997
      format('4')
                      SCURPLT. BXB
                                     Birkeland Current Distribution'
     write (6,*) '
     * // ' Plotter'
                                             Simple Model'
     write (6.*) '
     write (6,998)
      format ('2')
0998
     if (inter.eq.0) then
       fnum (1:2) =pfnum (1:2)
       cur-pour
       goto 2000
     endif
     WRITE (6,01000)
01000 FORMAT ('SEnter DIS.DAT version number [ integer ] : ')
     READ (6,01010) FNUM
01010 FORMAT (2A)
     MRITE (6,01020)
01020 FORMAT ( '$Enter Current Magnitude [ Real ] : ' )
     READ (6,*) CUR
02000 DARRAY (9:10) =FHUM (1:2)
     if (inter.eq.1) then
       write (6,*) 'File : ',darray(1:10)
       write (6, *) 'Current : ', cur
       write (6,*)
     endif
     OPEN (UNIT=1, NAME=DARRAY, TYPE='OLD')
     READ (1, *) NCODE, DF
      RRAD (1, *) CL1, CL2
```

```
READ (1,*) NUMT, NUML
     READ (1,*) (((TP(I,J,K), K=1,NUML), J=1,NUMT+1), I=1,4)
     READ (1,*) ((AMP(I,J,K), K=1,NUML), J=1,NUMT), I=1,2)
     CLOSE (UNIT=1)
С
     CALL CALCHP (X,Y,1,0)
     CALL CALCHO (X,Y,0,2)
     CALL WINDEW (0.,14.,-5.6,8.4,0.,11.,-5.5,5.5,1)
       call putinfo(darray(1:11),7.8,2.3,.10,.false.)
C **** LOOP 10000 DRAWS THE VECTORS AND THEIR HEADS ****
C
     DO 10000 I = 1, NUMT
        DO 10000 J = 1, NUML
C **** THIS PART DRAWS THE VECTORS. ****
F=(CL1+(2.*I-1.)*(CL2-CL1)/(2.*NUNT))/40.
           XL=-4.5*F*CO8(2.*(J-.5)*PI/HUML)
           YL=-4.5*F*SIM(2.*(J-.5)*PI/MUML)
           CALL CALCIEP (XL, YL, 0, 1)
           IF ((AMP(1,I,J)**2+AMP(2,I,J)**2).EQ.0.) GO TO 10000
           XP=XL+CUR*(AMP(1,1,J)*XL-AMP(2,1,J)*XL)/SQRT(XL**2+YL**2)
YP=YL+CUR*(AMP(1,1,J)*YL+AMP(2,1,J)*XL)/SQRT(XL**2+YL**2)
CALL CALCHD*(XF,YF,1,1)
C **** THIS PART DRAWS THE ARROW HEADS. ****
           TH=ATAM2((XF-XL),(YL-YF))
           X=XF-.06*SIB(TB-20.*PI/180.)
Y=YF+.06*COS(TB-20.*PI/180.)
           CALL CALCAD (X,Y,1,1)
           X=XF-.06*SIN(TH+20.*PI/180.)
           Y=YF+.06*COS(TH+20.*PI/180.)
           CALL CALCIER (X,Y,1,1)
           CALL CALCID (XF, YF, 1, 1)
10000 CONTINUE
C **** LOOPS 50000 AND 60000 DRAW THE LATITUDE CIRCLES ****
C *** AND MLT LIMES AND LABELS RESPECTIVELY.
     CALL CALCIER (0.,0.,0.1)
     CALL GRAIN (0.0)
      DO 50000 I = 1, 4
        PRAD=1.125*I
        CALL ARC (PRAD, 0., 360.)
50000 CONTINUE
      DO 60000 I = 1, 12
        ST=SIM((I-1)*PI/6.)
        CT=COS((I-1)*PI/6.)
        XL=4.5*CT
        YL=4.5*ST
        X=XL-3.375*CT
        Y=YL-3.375*8T
        CALL CALCID (X,Y,0,1)
        CALL CALCID (XL, YL, 1, 1)
        MLT=2.*(I-1)
        XN=XL+.7*CT+.105
        YN=YL+.7*8T-.07
        IF (MLT.GT.9) YM=YM-.14
        CALL NUMBER (XM, YM, .21, MLT, 90., -1)
60000 CONTINUE
```

```
C
      CALL CALCMP (7.5,-4.86,0,1)
      CALL CALCHP (7.0,-4.86,1,1)
     CALL CALCHP (7.05, -4.88,1,1)
     CALL CALCMP (7.05, -4.84,1,1)
     CALL CALCHP (7.0, -4.86,1,1)
     CURR=.5/CUR
     CALL SYMBOL (7.35,-4.7, 14,28= ,90.,2)
     CALL NUMBER (999., 999., 14, CURR, 90., 2)
     CALL SYMBOL (999., 999., .14, 4H AMP, 90., 4)
     CALL SYMBOL (6.4,-5.07,.28,16HDISTRIBUTION OF ,90.,16)
     CALL SYMBOL (999., 999., .28, 20HIONOSPHERIC CURRENTS, 90., 20)
     RCODE-MCODE
     CALL MUMBER (8.0,-5.07,.14,RCODE, 90.,0)
     CALL NUMBER (999.,999.,.14,CL1,90.,0)
     CALL MUMBER (999., 999., .14, CL2, 90., 0)
     RUMT-HUMT
      CALL NUMBER (999., 999., .14, RUMT, 90., 0)
     RUMI-MUMI.
     CALL MUMBER (999., 999., .14, RUML, 90., 0)
     CALL PAUS
     CALL CALCID (X,Y,1000,2)
C
C
      RETURN
     EMD
     program scurplt it
       call scurplt (T, ', 0.0)
        stop
```

# SBRKALC SOURCE CODE

```
SBRKALC, FOR
                                      Birkeland Current calculation
C
                        John L. Jamison for DM Klumpar
C
                       Lockheed Palo Alto Research Laboratory 0/91-20 B/255
c
                       June, 1988
C
  Revision history
   12-Jul-88
a
                       made into callable subroutine
•
     6-Jul-88
               JLJ
                       Added max to MRAS
C
    1-Jul-88
               JLJ
                       Debugging
   30-Jun-88
               JLJ
                        change ALTI from 140000, to 120000,
   30-Jun-88
                        added input value checking code
                        fixed prompt for altitude
α
                       initial entry
   29-Jun-88
Œ
        subroutine SBRKALC (inter, pfnum, palt, pincl, ptheta, pnmeas,
                               pifld, pipass)
        dimension fld(4), ftem(3)
c SBRK.INC defines the common block, and most of the shared data types
        include 'model: [simple] sbrk.inc'
        integer inter, pameas, pifld, pipass
        real palt, pincl, ptheta
        character*11 darray /'DIS.DAT; '/
        character*2 fnum, pfnum
        real#4 incl.mp
        data RE /6371000./
        data alt1 /120000./
        data pi /3.14159265/
        write (6,*)
        write (6,*) 'SRRKALC. EXR (Simple) Birkeland Current Generator'
        write (6,*)
        if (inter.eq.0) then
          fnum(1:2)=pfnum(1:2)
           alt=palt
           ipass= pipass
           ifld = pifld
           incl = pincl
           theta= ptheta
           nmeas- pomeas
           goto 2000
        2 ibae
        write (6,1000)
          format ('$Enter DIS.DAT version number: ')
 1000
        read (5, 1010)
 1010
         format (2a)
         format('$Enter Altitude [ RRAL, maters ] : ')
ead (5,*) alt
       write (6,1020)
 1020
        read (5,*) alt
   if inputted ALT is less than 10000, then its assumed that the
O
    user entered a RM value
a
        if (alt.gt.0.0.and.alt.lt.10000,) then
           write(6,*) 'Assuming Kilometers, adjusting...'
           alt=alt = 1000.
           write (6, 1019) alt
```

```
1019
            format (' Using ', f8.0,' meters for altitude.')
       endif
       write (6, 1021)
1021
       format('$Enter Inclination [ REAL, deg. from pole ] : ')
       read (5,*) incl
       write (6, 1022)
1022
        format ('$Enter Theta [ REAL, deg from dawn-dusk line ] : ')
       read (5, *) theta
1029 write (6, 1030)
1030 format (' &Rnter number of measurement points [ Integer,
         ,'<= 500 1 : ')
       read (5,*) nmeas
       if (nmeas.gt.500) goto 1029
1039 write (6, 1040)
 1040
         format (' Enter 1 for the Field of all currents'/
                       2 for Field-Aligned only'/
                    3 for Morth-South only'/
                       4 for East-West only'/
                       5 for Ring current only'/
                18> 1)
       read (5,*) ifld
       if (ifld.lt.l.and.iflt.gt.5) goto 1039
 1049 write (6, 1050)
         format (' Enter 1 for Polar'/
 1050
                      2 for Equatorial West'/
                       3 for Equatorial East'/
                18> 1
       read (5,*) ipass
       if (ipass.lt.0.and.ipass.gt.3) goto 1049
       if (ipass.eq.0) ipass=1
c BOTE use of funD for Degrees, rather than fun for Radians
 2000 darray (9:10) = fnum (1:2)
       if (inter.eq.1) then
                            : ',darray(1:10)
          write(6,*) 'File
                               alt
          write(6,*) 'Alt
          write(6,*) (Ipass
                               ipass
                               111d
          write(6, *) / Ifld
                              ',incl
          write(6,*) 'Incl
          write(6,*) 'Theta : ',theta
          write(6,*) 'Nmeas
                               , nmeas
          write(6,*)
       endif
        st= sinD(theta)
       ct = cosD(theta)
       sincl = sinD(incl)
       cincl = cosD(incl)
       open (unit=1.name=darray.type='old')
  following read statements match CURDIS.FOR (Simple) WRITES JLJ
a
        read (1,*) ncode, df
       read (1,*) cl1, cl2
        read (1,*) numt, numl
       n = numt + 1
```

```
read (1,*) (((tp(i,j,k), k=1,numl), j=1,n), i=1,4)
read (1,*) (((amp(i,j,k), k=1,numl), j=1,numt), i=1,2)
         read (1,*) ((rzf(i,j), j=1,n), i=1,2)
         read (1,*) ((rb(1,j), j=1,n), i=1,2)
read (1,*) ((rt(1,j), j=1,n), i=1,2)
read (1,*) (rxi(k), k=1,numt)
         read (1,*) (rze(i), i=1.numt)
         read (1.*) (re1(i), i=1, numt)
         read (1,*) ((ri(i,j), j=1,numt), i=1,2)
        read (1,*) ((scl(i,j), j=1,n), i=1,2)

read (1,*) ((ccl(i,j), j=1,n), i=1,2)

read (1,*) ((smi(i,j), j=1,n), i=1,2)

read (1,*) ((smi(i,j), j=1,n), i=1,2)

read (1,*) ringe, ringb
         read (1, *) (tpr(i), i=1, numl)
         read (1,*) (ampr(1),1=1,numl)
         close (unit=1)
         open (unit=1, name='mag.dat', type='new')
         write (1.*) pcode.alt
         write (1, *) incl. theta
         write (1,*) cl1,cl2
         write (1,*) numt, numl
         write (1,*) nmeas,ifld
         write (1, *) ipass
   loop 1000 determines {X,Y,Z} coords of each measurement point and calls
    MACHOD to obtain Field parameters for each point
         do 10000 lxwl; nmeas, the second
                   m_0 = (1.-(lx-1)*2./(nmeas-1))*pi*40./180.
                   -(ipass-1)*270.*pi/180.
                   ann = sin(mp)
                   comp = cos(mp)
                   xl=(re+alt)*(-st*smp+ct*cmp*sincl)
                   yl=(re+alt) * (ct*amp+at*cmp*sincl)
                   sl=(re+alt) +cmp*cincl
  xl,yl,zl = {X,Y,Z} of measurement point
               = the three components of dB and FAC determined from MAGMOD
   fld
               m tells magmod which current systems to include when crunching away
   1fld
                   call magmod(xl,yl,zl,fld,ifld)
                   write(1.*) fld
10000
         continue
         close (unit=1)
         return
         end
         program sbrkalc it
         call sbrkalc(1, ',0.0,0.0,0.0,0,0,0)
         stop
         end
```

## SMAGMOD SOURCE CODE

```
SMAGMOD . FOR
                          Magnetic Field Model
C
C
                         John L. Jamison
C
                         Lockheed Palo Alto Research Laboratory 0/91-20 B/255
С
С
        Revision History,
C
        7/14/88 JLJ
                        created LAMBDAS lookup table for lambda values
C
C
        7/1/88 JLJ
                        debugging
        6/29/88 JLJ
C
                        initial entry
c
0
a
C
C**
C
      subroutine magmod (x1, y1, z1, fld, ifld)
O
a
  **** calculates current density and magnetic field components
  **** of birkeland current model defined by curdis.
0
0
C
٥
      include 'model: [simple] sbrk.inc'
      dimension famp(21,24),rm(3,3),fld(4)
      dimension bf(3), btf(3), bti(3), bte(3), btr(3)
      real*4 lambda, mp, jt
      data pi / 3.14159265 /
      real*4 lambdas(24)
                               [1..numl]
c create lambdas lookup table, because they're always calculated the same way
      do j=1, numl
        lambdas(j)=2.*(j-.5)*pi/numl
      end do
O
      do 100001 = 1.3
         btf(1) = 0,
         bti(1) = 0.
         bte(1) = 0.
         btr(1) = 0.
10000 continue
      jt = 0.
      if (ifld.eq.-2) go to 03000
      if (ifld.gt.2) go to 03000
•
  **** loop 20000 does the field aligned currents supplying
c **** both the e-w and n-s ionospheric currents.
g **** positive current is vertical.
      1=numt+1
      do 20000 = 1, 2
         if (m.eq.2) i=numt
         do 20000 n = 1, 1
            do 20000 1=1, numl
            if (m.eq.2) goto 20010
            famp(1, 1) = amp(1, 1, 1)
            famp (numt+1, j) =-amp (1, numt, j)
            if (n.eq. (numt+1)) goto 20020
            if (n.gt.1) famp (n, j) = amp(1, n, j) - amp(1, n-1, j)
            if (famp(n, j).eq.0.) goto 20000
```

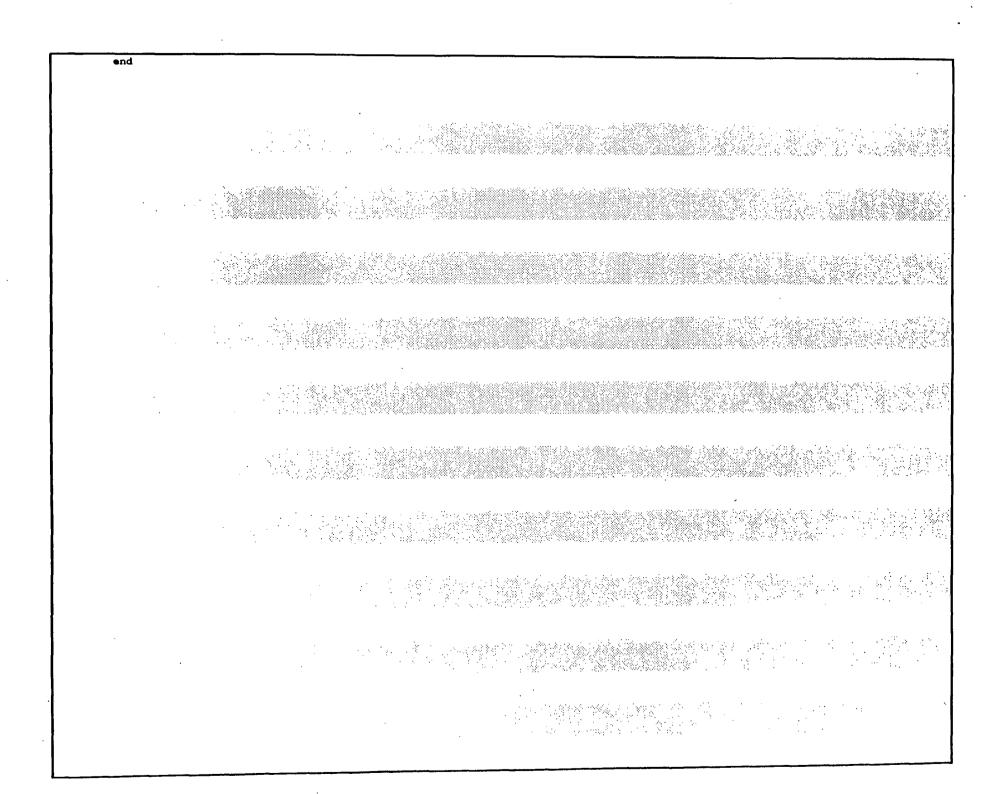
```
goto 20020
20010
            famp(n, 1) = amp(2, n, numl) - amp(2, n, 1)
            if (j.gt.1) famp(n, j) = amp(2, n, j-1) - amp(2, n, j)
            if (famp(n, j).eq.0) goto 20000
c rearranged and optimized, JLJ
            lambda=2.*(j-.5)*pi/numl
if (m.eq.2) lambda=2.*j*pi/numl
c20020
c
20020
            if (m.ne.2) then
               lambda = lambdas(1)
            else
               lambda = 2.*j*p1/numl
            endif
            sla = sin(lambda)
            cla = cos(lambda)
            rm(1,1) = cla * com(m,n)
            r=(1,2) = ala*cmu(n,n)
            ra(1,3) = -smi(n,n)
            rm(2,1) = -sla
            rm(2,2) = cla
            rm(2,3) = 0.
            rm(3,1) = cla*emn(m,n)
            rm(3,2) = sla*smu(m,n)
            ra(3,3) = canu(a,n)
           xf = xl*rm(1,1) + yl*rm(1,2) + (xl-rxf(m,n))*rm(1,3)

yf = xl*rm(2,1) + yl*rm(2,2) + (xl-rxf(m,n))*rm(2,3)

xf = xl*rm(3,1) + yl*rm(3,2) + (xl-rxf(m,n))*rm(3,3)
a
            rcf = xf**2 + yf**2
            rbf = aqrt(rcf + (sf-rb(m,n))**2)
            rtf = sqrt(rof + (rf-rt(m,n))**2)
           byf = -famp(n, j) * (tanh(rcf*tp(m, n, j))) * (xf/rcf)
     1
                  *((rt(m,n)-rf)/rtf + (rf-rb(m,n))/rbf)
           do 21000 ip = 1,3
bf(ip) = hxf*rm(1,ip) + byf*rm(2,ip)
              btf(ip) = btf(ip) + bf(ip)
21000
            continue
            if ((tp(m,n,j)*rcf) .gt. 40.) go to 20000
            write (6,*) [------
            write (6,*) 'M, M, J = ', m, n, j
write (6,*) 'famp(n,j) = ', famp(n,j)
            write (6,*) 'tp(m,n,j)= ',tp(m,n,j)
            write (6,*) 'pi
                                = ',pi
                                 = ',rcf
            write (6, *) 'rcf
                                 · file of the property of the pro-
            write (6, #) 'jt
                               = ', cosh (tp(m,n,j) *rcf)
            write (6,*) 'cosh
            jt = famp(n,j)*tp(m,n,j)
               /(pi*((cosh(tp(m,n,j)*rcf))**2)) + jt
20000 continue
     if (ifld.eq.2) go to 07000
03000 if (ifld.eq.5) go to 04000
c
```

```
do 30000 n = 1, numt
         do 30000 j \approx 1, numl
c
             lambda = 2.*(j-.5)*pi/numl
            lambda=lambdas(1)
            sla = sin(lambda)
            cla = cos(lambda)
            rm(1,1) = cla*ccl(2,n)
            rm(1,2) = sla*ccl(2,n)
            rm(1,3) = -scl(2,n)
            rm(2,1) = -sla
            rm(2,2) = cla
            xm(2,3) = 0.
            rm(3,1) = classcl(2,n)
            rm(3,2) = sla*scl(2,n)
            rm(3,3) = ccl(2,n)
            1f (1fld.eq.-3) go to 30100
            if (ifld.eq.4) go to 30100
  **** this part does the north-south ionospheric currents.
  **** negative current is northward.
            12(amp(1, n, j) .eq. 0.) go to 30010
            xf = xl*rm(1,1) + yl*rm(1,2) + (xl-rzi(n))*rm(1,3)
            yf = xl*rm(2,1) + yl*rm(2,2) + (xl-rxi(n))*rm(2,3)
            xf = xl*rm(3,1) + yl*rm(3,2) + (xl-rxi(n))*rm(3,3)
            rof = yf**2 + #f**2
            ril = sqrt(rof + (xf - ri(1,n))**2)
            ri2 = sqrt(rof + (xf - ri(2,n))**2)
            byf = -amp(1,n,j)*(tanh(100.*rof*tp(3,n,j)))*(xf/rof)
                  *(((xf-ri(1,n))/ril) + (ri(2,n)-xf)/ri2)
            bsf = asp(1,n,j)*(tanh(100.*rof*tp(3,n,j)))*(yf/rof)
                  +(((xf-ri(1,n))/ri1) + (ri(2,n)-xf)/ri2)
            do 31000 ip = 1,3
               bf(ip) = byf*rm(2,ip) + bzf*rm(3,ip)
               bti(1p) = bti(1p) + bf(1p)
            continue
31000
30010
            continue
            if (ifld.eq.-4) go to 30000
            1f (1fld.eq.3) go to 30000
o **** this part does the east-west electrojets.
C **** positive current is eastward.
            1f(amp(2,n,j) .eq. 0.) go to 30000
30100
            xf = xl*rm(1,1) + yl*rm(1,2) + zl*rm(1,3)
            yf = x1*rm(2,1) + y1*rm(2,2) + x1*rm(2,3)
            zf = x1*rm(3,1) + y1*rm(3,2) + z1*rm(3,3)
            rof = xf**2 + (xf - rse(n))**2
            rel = sqrt(ref + (yf + rej(n))**2)
            re2 = sqrt(rof + (yf - rej(n))**2)
            bxf = amp(2, n, j)*(tanh(100.*rcf*tp(4, n, j)))
```

```
*(zf-rze(n))*((yf+rej(n))/rel+(rej(n)-yf)/re2)/rcf
           bzf = -amp(2, n, j)*(tanh(100.*rcf*tp(4, n, j)))
            *xf*((yf+rej(n))/rel+(rej(n)-yf)/re2)/rcf
            do 32000 ip = 1,3
              bf(ip)=bxf*rm(1,ip) + bzf*rm(3,ip)
              bte(ip) = bte(ip) + bf(ip)
32000
           continue
30000 continue
¢
      if (ifld.la.1) goto 04000
      if (ifld.lt.5) goto 07000
04000 if (ifld.eq.-5) goto 07000
c **** loop 40000 calculates field due to ring current
     do 40000 1=1, numl
       lambda=2.*(1-.5)*p1/mml
C
       lambda=lambdas(1)
       sla=sin(lambda)
       cla=cos(lambda)
o
       rm(1,1)=cla
       rm(1,2)=ela
       x=(1,3)=0.
       rm(2,1)=-sla
       zm(2,2)=cla
       ra(2,3)=0.
       rm(3,1)=0.
       x=(3,2)=0.
       rm(3,3)=1.
C
       if (ampr(i).eq.0.) goto 40000
O
       xf=x1*rm(1,1) + y1*rm(1,2) + x1*rm(1,3)
       yf=x1*rm(2,1) + y1*rm(2,2) + x1*rm(2,3)
       sfemitrm(3,1) + yltm(3,2) + mltm(3,3)
O
        rof=(xf-ringa)**2 + xf**2
       rrl=eqrt (rcf+(yf+ringb) **2)
       rr2=aqrt (rof+ (yf-ringb) **2)
0
       bxf=ampr(1) * (tanh (rof*tpr(1))) ***f
          *((yf+ringb)/rrl+(ringb-yf)/rr2)/rcf
       brf=-ampr(i) * (tanh(rof*tpr(i))) * (xf-ringa)
           *((yf+ringb)/rrl+(ringb-yf)/rr2)/rcf
a
        do 41000 1p=1,3
          bf(ip)=bxf*rm(1,ip)+bxf*rm(3,ip)
          btr(1p)=btr(1p)+bf(1p)
41000
       continue
40000 continue
o **** loop 70000 adds fields from all sources and converts to a 1.
07000 \text{ do } 70000 \text{ ip} = 1,3
        fld(ip) = 200.*(btf(ip)+bti(ip)+bte(ip)+btr(ip))
70000 continue
      fld(4) = jt
return
```



## SBRKPLT SOURCE CODE

```
SBRKPLT
                       Bierkland Current density plotter
C
c
                       JL Jamison, for DM Klumpar
                       Lockheed Palo Alto Research Laboratory
C
c
                       O/91-20 B/255
a
       Revison History
^
^
       7/12/88 JTJ
                       made into callable subroutine
•
       7/2/88 JLJ
C
                       cleaned up input prompting
       7/1/88 JLJ
                       debugging
        6/30/88 JIJ
                       Initial integration into "Simple" system
                       changed ALTI from 140000. to 120000
C **** BREPLT PLOTS CURRENT DENSITY AND FIELD COMPONENTS
C **** FOUND BY BREALC.
C
      subroutine sbrkplt (inter.pfnum, pmode)
      DIMENSION FL(4,500), FTEM(3), FACT(4), FLD(4)
      DIMENSION PHAX (4)
      LOGICAL*1 ATEX (16), TEXT (8)
      character*11 darray /'MAG.DAT; '/
      character*2 fnum.pfnum
      integer prode, inter
     REAL®4 ILAT, INCL. JT. JTMAX, MLT. MP. MAT
      DATA PI / 3.14159265 /
      DATA RE / 6371000. /
      DATA ALTI / 120000. /
     C
      write (6,997)
       format ('4')
0997
                                      Birkeland Current Plotter
      write (6,*) '
                      SERRELT. EXE
      write (6,*) '
      write (6,998)
      format ('2')
0998
      if (inter.eq.0) then
       f_{num}(1:2) = pf_{num}(1:2)
       mode = pmode
       goto 2000
      endif
      WRITE (6,01000)
01000 FORMAT ('SEnter MAG.DAT version number [ Integer ] : ')
      READ (6,01010) FNUM
01010 FORMAT (2A)
01015 write (6,*) 'Select Coordinate system:'
      WRITE (6,01020)
01020 FORMAT ('$Enter 1 for XYZ; 2 for MEV; 3 for SDV; '
               ,'4 for ABZ [ Integer ] : ')
      READ (6, *) MODE
      if (mode.lt.l.and.mode.gt.4) goto 1015
```

```
02000 darray (9:10) = fnum (1:2)
     if (inter.eq.1) then
        write (6,*) 'File : ', darray(1:10)
        write (6,*) 'Mode : ', mode
        write (6,*)
     endif
     OPEN (UNIT-1, NAME=DARRAY, TYPE='OLD')
     READ (1, *) NCODE, ALT
     RRAD (1, *) INCL, THETA
     RRAD (1,*) CL1, CL2
     RRAD (1,*) NUMT, NUME.
     READ (1,*) MORAS, IFLD
     READ (1,*) IPASS
     DO 10000 J = 1, NMRAS
        READ (1, *) FLD
        DO 10000 I = 1.4
          YL(I,J) = YLD(I)
10000 CONTINUE
     CLOSE (UNIT=1)
C
     SINCL = SIN (PI*INCL/180.)
     CINCL = COS (PI*INCL/180.)
     87 = SIN (PI*THETA/180.)
     CT = COS(PI*THETA/180.)
C
     IF (MODE .LE. 1) GO TO 11111
C
 **** CONVERT TO MEV ON 2; SDV ON 3; ARE ON 4
C
     DO 11000 J = 1, NMRAS
        MP = (1.-(J-1)*2./(NMCAS-1))*PI*40./180.
            -(IPASS-1) *270. *PI/180.
        SIG = SIM (ICP)
        CMP = COS (MP)
        XL = -ST*SMP + CT*CMP*SINCL
        YL - CT+SMP + ST+CMP+SINCL
        IL = CMP*CINCL
        PTEM(1) = PL(1,J)
        FTEM(2) = FL(2,J)
        \mathbf{FTEM}(3) = \mathbf{FL}(3,J)
        Q1 - SQRT(XL**2 + ZL**2)
        Q2 = SQRT(YL**2 + ZL**2)
        Q3 = SQRT(XL**2 + YL**2)
C
        FL(3,J) - -FTEM(1) *XL - FTEM(2) *XL - FTEM(3) *&L ...
C
        IF (MODB .EQ. 3) GO TO 11010
C
        YL(1,J) = -YTRM(1) *XL*ZL/Q3 - YTRM(2) *YL*ZL/Q3 + YTRM(3) *Q3
        FL(2,J) = -FTRM(1)*YL/Q3 + FTRM(2)*XL/Q3
        IF (MODE .BQ.2) GO TO 11000
        PTRM(1) = PL(1,J)
        PTEM(2) = PL(2,J)
        FL(1,J) = FTEM(1)*COS(PI/60.) - FTEM(2)*SIN(PI/60.)
        FL(2, J) = FTEM(1)*SIN(PI/60.) + FTEM(2)*COS(PI/60.)
        GO TO 11000
                                                                 FL(1,J) = (FTEM(1)*ZL + FTEM(3)*XL)/Q1
11010
        FL(2,J) = (-FTRM(2)*ZL - FTRM(3)*YL)/Q2
11000 CONTINUE
С
```

```
C **** FIND MAXIMA
11111 DO 12000 I = 1.4
       DO 12000 J = 1, NMEAS
         FMAX(I) = AMAX1(ABS(FL(I,J)),FMAX(I))
12000 CONTINUE
    PMAX (1) =AMAX1 (PMAX (1), FMAX (2))
    FHAX (2) =FHAX (1)
C
    CALL CALCHE (X,Y,2,0)
     CALL CALCHY (X, Y, 0, 2)
C
C **** PLOT BACKGROUND
C
    xorg=0.
    yorg=0.
    call calcomp (xorg, yorg, 0,3)
    call putinfo(darray(1:10),13.0,1.0,0.10,.false.)
    XORG = .15
     YORG = .1
     CALL CALCIE (XORG, YORG, 0, 3)
     DO 20000 I = 1,9
       Y = (I-1)*1.2 + .8
       CALL CALCIUP (X, Y, 0, 1)
       Y = (I-1)*1,2 + .8
CALL CALCEP (X;Y,1,1)
IF (I .BQ. 9) GO TO 20000
       DO 20000 J = 1,18
          IF (J . GT. 9) H = J - 9
         XL = 1.
          IF (J . GT. 9) XL = 10.9
         X - XL
          Y = (M/10. + I - 1)*1.2 + .8
         CALL CALCID (X, Y, 0, 1)
         X = .1 + XL
         Y = (W/10. + I - 1) + 1.2 + .8
CALL CALCAD (X.Y.1.1)
20000 CONTINUE
C
 **** INDICATE GEOLAT, INVLAT, MLT
C
    goto 30000
    DO 30000 I = 1, 6
       DO 30000 J = 5, 85, 5
         G = (45-J)*PI/180.-(IPASS-1)*270.*PI/180.
QJ = 1.*J + 5.
BG = BIN(G)
          BG = BIM(G)
         CG = COS(G)
          YL = -ST*SG + CT*CG*SINCL
          YL = CT*SG + ST*CG*SINCL
          EL = CG*CINCL
         RL = SORT(XL**2 + YL**2)
C
         GLAT = 180.*(ACOS(SQRT(XL**2+YL**2)))/PI
         GLATR = GLAT*PI/180.
         ILAT = 180. * (ACOS ((SQRT (RE/(RE+ALT))) *COS (GLATR)))/PI
```

```
С
            MLT = ASIN(YL/RL)*12./PI + 12.
            IF ((XL .LT. 0.) .AND. (YL .GT. 0.))
            MLT = ASIN(-XL/RL)*12./PI + 18.
            IF ((XL .LT. 0.) .AND. (YL .LT. 0.))
            MLT = ASIN(-YL/RL)*12./PI
            IF ((XL .GT. 0.) .AND. (XL .LT. 0.))
            \mathbf{MLT} = \mathbf{ASIH}(\mathbf{XL/RL}) * 12./\mathbf{PI} + 6.
C
            W = 6. - (G+(IPASS-1)*270.*PI/180.)/.13962641
            IF (I .RO. 6) GO TO 30010
            H = (I-1)*2.4 + .8
            Y = - 05 + H
            CALL CALCHE (X, Y, 0, 1)
            Y = .05 + H
            CALL CALCIER (X,Y,1,1)
            GO TO 30000
30010
            IF (ABS (AMOD (GJ, 10.)) .GT. 0.) GO TO 30000
            H = .8
            XM = W - .29
            YM = H - .24
            CALL NUMBER (XN, YN, .14, GLAT, 0., 2)
            YH = H - .45
            CALL NUMBER (XM. YM. .14. ILAT, 0..2)
            YN - H - .66
            CALL NUMBER (XH, YH, .14, MLT, 0., 2)
30000 CONTINUE
C
C
  **** DRAW LATITUDE CIRCLES
C
C
      CHORM-SIN (40.*PI/180.)
       CALL CALCAR (12.9, 8.7, 0, 3)
a
      CALL CALCAD (12.7.8.7.0.3)
      CALL CALCID (0.,0.,0,1)
      CALL GRAIM (0.0)
      IF (IPASS.GT.1) GO TO 04200
      DO 40000 I = 10,40,10
         PRAD=SIN(I*PI/180.)/CMORM
         CALL ARC (PRAD, 0., 360.)
40000 CONTINUE
C **** OR EQUATORIAL VIEW OF THE EARTH
      IF (IPASS.EQ.1) GO TO 05000
04200 CALL CALCAD (X, Y, 1, -5)
      DO 42000 I=1.9
         CRAD=COS ((I-5)*PI/18.)
         X=SIH((I-5)*PI/18.)/CNORM
         Y-CRAD/CHORM
         CALL CALCOR (X,Y,0,1)
         Y=-CRAD/CHORM
         CALL CALCIE (X,Y,1,1)
42000 CONTINUE
      DO 43000 I=10,190,10
         CRAD=COS((I-10)*PI/180.)
          DO 43000 J=1,81
            X=SIN((J-41)*PI/180.)/CNORM
            Y=CRAD*COS ((J-41)*PI/180.)/CNORM
            IF (J.EQ.1) CALL CALCHP (X,Y,0,1)
```

```
CALL CALCMP (X,Y,1,1)
43000 CONTINUE
     CALL CALCHP (X,Y,0,-5)
c
C **** INDICATE TIME
05000 CALL CALCHE (XORG. YORG. 0.3)
     IP=1
     IF (IPASS.GT.1) IP=2
     DO 50000 I = 1, 4
        s = sin((i-1.)*pi/2)
        C = COS((I-1.)*P1/2.)
        IF (IPASS.GR.2) GO TO 50001
        X = .25*S + 12.75
C
        X = .25*S + 12.55
        Y = -.25 * C + 8.6
        CALL CALCOR (X.Y.O.1)
a
         X m S + 12 75
        X = 8 + 12.55
        Y = -C + 8.6
        CALL CALCHE (X.Y.1.1)
50001
        RMDM = (T-1)*6.
        GO TO (50010,50020,50030,50040) I
c50010
        XL = 12.72
50010
        XL = 12.52
        YL = 7.4 - (IP-1) * .6
        CALL NUMBER (XL, YL, .14, RNUM, 0., -1)
        GO TO 50000
o50020
        XL = 13.82
50020
        XL = 13.62
        TL = 8.53
        IF (IPASS.GR.2) GO TO 50021
        CALL NUMBER (XL, YL, .14, RNUM, 0., -1)
        GO TO 50000
        CALL SYMBOL (XL, YL, .14, 1HM, 0.,1)
50021
        GO TO 50000
c50030
         XL = 12.63 + (IP-1) * .001
50030
        XL = 12.43 + (IP-1) * .001
        YL = 9.67 + (IP-1)*.6
        CALL NUMBER (XL, YL, .14, RNUM, 0., -1)
        CO TO 50000
o50040
        XL = 11.45 + (IP-1) * .18
        XL = 11.25+(IP-1)*.18
50040
        YL = 8.53
        IF (IPASS.GE.2) GO TO 50041
        CALL NUMBER (XL, YL, .14, RNUM, 0., -1)
        CO TO 50000
50041
        CALL SYMBOL (XL, YL, .14, 185, 0., 1)
50000 CONTINUE
C **** PLOT ORBIT
06000 DO 60000 I = 1, MGRAS
        MP = (1.-(1-1)*2./(MGAS-1))*PI*40./180.
          -(IPASS-1) *270. *PI/180.
        SMP = SIN (MP)
        CDOP = COS(MP)
        XL = -ST*SMP + CT*CMP*SINCL
        YL = CT*SMP + ST*CMP*SINCL
        IL = CMP*CINCL
         X=-YL/CNORM+12.75
a
        X=-YL/CNORM+12.55
```

```
Y= XL/CNORM+8.6
C
         IF (IPASS.GE.2) X=ZL/CNORM+12.75
        IF (IPASS.GR.2) X=ZL/CNORM+12.55
        IF (I .EQ. 1) CALL CALCMP (X, Y, 0, 1)
        CALL CALCHP (X,Y,1,1)
60000 CONTINUE
C
      IF (MODE .GT. 1) GO TO 07000
C
С
  **** SHOW X,Y VECTORS
C
a
      X = 11.58 ··
     X = 11.38
     Y = 9.07
     CALL CALCIOP (X, Y, 0, 1)
      X = 11.98
O
     X = 11.98-0.2
     Y = 9.07
      CALL CALCOR (X, Y, 1, 1)
      X = 11.98
O
     X = 11.98-0.2
     Y = 9.47
      CALL CALCIO (X, Y, 1, 1)
      CALL SYMBOL (11.82, 9.5, .14, 18x, 0., 1)
a
     CALL SYMBOL (11.82.9.5-0.2.14.1HX.0.,1)
C
      CALL SYMBOL (11.42, 9.07, .14, 187, 0., 1)
      CALL SYMBOL (11.42, 9.07-0.2, .14, 1HY, 0., 1)
C
C **** INDICATE MAXIMA
C
07000 IPLT-4
      IF (IFLD.EQ.-2) IPLT=3
      IF (IFLD.GT.2) IPLT=3
     DO 70000 I = 1. IPLT
        IF (I.ME, 4) GO TO 70005
        IF (FMAX (4) .NE.O.) GO TO 70005
        IDEC=-1
        ITY=1
        PACT(I)=1.
        GO TO 70065
        IF (I.EQ.4) FRAX(I)=FRAX(I)*1000000.
70005
        IDEC=-1
        IF (FMAX(I).LT.10.) IDEC=1
        IF (FMAX(I).LT.1.) IDEC=2
        IF (FRAX(I).LT..1) IDEC=3
        FACT(I)=1.
        IF (PIGE (I) .GE .10.) GO TO 70020
70010
        IF (FMAX(I).LT.1.) GO TO 70030
        IF (FMAX(I).GB.1.) GO TO 70040
        FACT (I) = FACT (I) /10.
70020
        PMAX (I) = FMAX (I) /10.
        GO TO 70010
70030
        FACT(I)=FACT(I)*10.
        FMAX (I) =FMAX (I) *10.
        GO TO 70010
        IF (INT(FMAX(I)).LT.INT(FMAX(I)+.5)) GO TO 70050
70040
        PMAX (I) = (AINT (FMAX (I))+.5) /FACT (I)
        GO TO 70060
        FMAX (I) =AINT (FMAX (I) +.5) /FACT (I)
70050
        IF (FWAX(I).LT.1000.) ITY=1
70060
        IF (FMAX(I).LT.100.) ITY=2
```

```
IF (FMAX(I).LT.10.) ITY=1
        IF (FMAX(I).LT.1.) ITY=1
        IF (FMAX(I).LT..1) ITY=-1
        IF (FMAX(I).LT..01) ITY=-2
70065
        XL = 1.2
        YL = (5-1)*2.4 + .4
        N = I + (MODB-1)*4
        CALL SYMBOL (XL, YL, .28, ATRX (N), 0, .1)
        IF (I .BQ. 4) CALL SYMBOL (999.,999.,.1,1HV,0,1)
        XL = ITY^*.14+.4
        YL = (5-1)*2.4 + .6
        CALL NUMBER (XL, YL, .14, PMAX(I), 0., IDEC)
        FM = 0.
        XI.m. 8
        YL = (5-1)*2.4 + .47
        CALL NUMBER (XL, YL, .14, YM, 0., -1)
        PM=-PMAX(I)
        XL=ITY*.14+.26
        IF (PMAX(I).BQ.0.) XL-XL+.14
        YL = (5-1)*2.4 - 1.55
        CALL NUMBER (XL, YL, .14.FM, O., IDEC)
        XL=.2
        YL=(5-1)*2.4-1.1
        IF (I.BQ.4) GO TO 70070
        CALL SYMBOL (XL, YL, 14, 10HNAMOTESLAS, 90, 10)
        GO TO 70080
70070
        YL=YL-.15
        CALL SYMBOL (XL, YL, .14, 11HMICROAMPS/M, 90., 11)
        XL=XL-.1
        YL=YL+1.54
        CALL SYMBOL (XL, YL, . 07, 1H2, 90., 1)
        IF ((I.EQ.4).AND. (FMAX(I).EQ.0.)) GO TO 70000
70080
        IF (I.RQ.4) FMAX(I) =FMAX(I)/1000000.
70000 CONTINUE
C
C **** PLOT FIELDS
C
     DO 80000 I = 1, IPLT
        IF ((I.EQ.4).AND. (ALT.LT.ALTI)) GO TO 80000
   don't plot if FMAX(I) = 0.0, otherwise bombs out with FLTDIVZER
        1f (fmax(1).eq.0.0) goto 80000
        DO 80000 J = 1, MMRAS
           MP = (J-1)*2./(NMRAS-1)
           X = 5.*MP + 1.
           X = 5. MF T 1.

Y = 2.4*(4-I) + 2. + 1.2*FL(I,J)/FMAX(I)

IF (J .EQ. 1) CALL CALCAP(X,Y,0,1)
           IF (J .EQ. 1) GO TO 80000
           CALL CALCIO (X, Y, 1, 1)
BOCOO CONTINUE
C
CALL CALCAGE (0.,0,,0,3)
     CALL STMBOL(0.,10.64,.35,21HB-FIELD OF BIRKELAND ,0.,21)
     CALL SYMBOL (999., 999., .35, 13HCURRENT MODEL, 0., 13)
     CALL SYMBOL (0., .66, .14, 6HGEOLAT, 0., 6)
     CALL SYMBOL (0., 0.45, .14, 6HINVLAT, 0., 6)
     CALL SYMBOL (0., 0.24, .14, 3HMLT, 0., 3)
     ORY=7.2
     IF (IPASS.GE.2) ORY=6.5
     CALL SYMBOL (12.55, ORY, .14, 5HORBIT, 0.,5)
     CALT = ALT/1000.
```

```
CALL SYMBOL (11.7, 6.0, .14, 17HALTITUDE =
                                               KM, 0., 17)
      CALL NUMBER (13.2, 6.0, .14, CALT, 0., -1)
      RCODE = NCODE
      CALL NUMBER (12.,0.,.14, RCODE, 0.,0)
      CALL NUMBER (999., 999., .14, CL1, 0., 0)
      CALL NUMBER (999., 999., .14, CL2, 0., 0)
      RUMT-NUMT
      CALL NUMBER (999., 999., .14, RUNT, 0., 0)
      RUML-NUML
      CALL NUMBER (999., 999., .14, RUMI, 0., 0)
     RFLD=IFLD
     CALL NUMBER (999., 999., .14, RFLD, 0., 0)
C
C
     CALL PAUS
     CALL CALCID (X,Y,1000,2)
C
     RETURN
     EDID :
     program sbrkplt it
       call abrkplt(I,' ',0)
       stop
      end
```